

# Model Validation Protocol toward MAPOD Application\*

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MAPODWG, Las Vegas, NV



# Outline

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## 1. Introduction

## 2. Model Validation Protocol

- Working protocol
- Salient features

## 3. Exercising the Validation Protocol

- Examples

## 4. Conclusions

# Introduction

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## Objective

- To develop and validate an eddy current (EC) model, aiming toward model applications to airframe inspections.

## Scope

- Model development and validation
- Development of a validation protocol = guidelines for validation procedure.

## Expected Significance

- The validation procedure will become an integral part of model-assisted POD (MAPOD) methodologies.

# Approach

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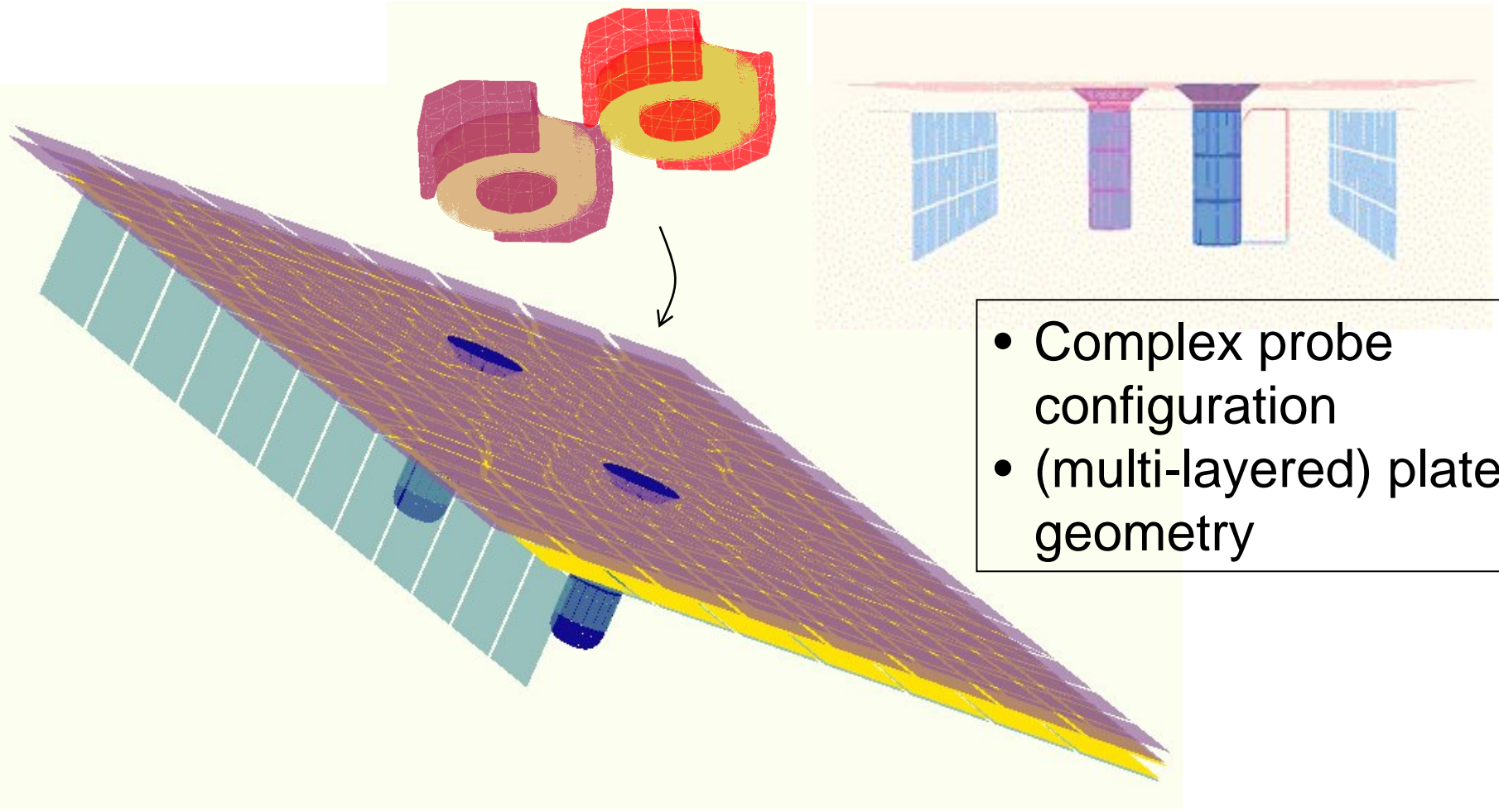
- Develop (draft) validation protocol
  - based on prior experience in industrial inspections and laboratory measurements.
- Exercise the protocol, and refine it through this exercise.
  - Select prototypical airframe eddy current inspections.
  - Select a BEM-based EC model (additional development)
  - Prepare sample (select, fabricate, and characterize)
  - Perform validation measurements & model calculations for comparison

# Considerations Prior to Exercising the Protocol

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- Select a test problem
  - EC inspections to test
  - Laboratory or Industrial problem
- Select a model to use
  - EC simulation model
  - Based on application requirement
- Determine precision requirements
  - Default accuracy (e.g. “ $\pm 10\%$ ”)
  - Based on application scope
    - Ex. MAPOD

# Inspection Configuration Example



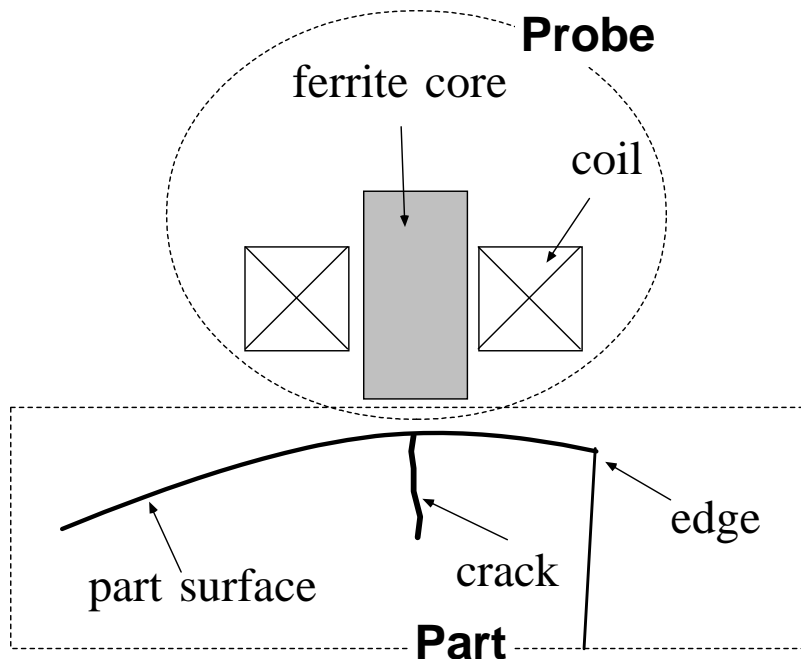
- Complex probe configuration
- (multi-layered) plate geometry

Cessna Aircraft

# Model Example: CNDE EC Models

## Physics-based models

- Idealize the system of an EC probe and parts



## • Modeling Algorithms

- **Analytical methods**
  - Dodd-Deeds Solution
- **Numerical methods**
  - Finite Difference
  - Finite Element
  - Volume Integral
  - Boundary Element
  - Hybrids

Auld's reciprocity formula

$$\begin{aligned}\Delta Z &= \frac{1}{I^2} \int_S d\vec{S} \cdot [\vec{E} \times \vec{H}' - \vec{E}' \times \vec{H}] \\ &= \frac{-1}{I^2} \int_V dV [\Delta\sigma(\vec{E} \cdot \vec{E}') + i\omega\Delta\mu(\vec{H} \cdot \vec{H}')] \end{aligned}$$

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- 2. Model Validation Protocol**
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# Model Validation Protocol

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- Purpose of the protocol
  - To ensure consistency of model validation procedure by providing guidelines for measurement and computation
- Functions of the protocol
  - “Measurement” protocol: guidelines for
    - Specimens to prepare/procure
    - Instrumentation (instrument & probe) to use
    - Data to acquire/record in what procedure
  - Guidelines to determine
    - What output signals to compute, compare with what data
    - What input parameters are needed, and how to determine
    - How to compare the model output to the data

# Validation Protocol, Draft Documents

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- Engine Applications
  - 10-page draft document
    - Including 6-page model-to-expt. calibration procedure
  - P&W - EC Model Validation Protocol
- Airframe Applications
  - 2-page draft document
  - Validation Protocol - Cessna

# Focal Points of Validation Protocol

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- Sample definition, procurement/fabrication
  - **Material property determination**
    - Sample to sample
  - **Defect Characterization**
    - Close to ideal defects
  - **Capture sample geometry/dimension data**
    - With idealization

# Focal Points of Validation Protocol (contd.)

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- Selection and characterization of instrumentation
  - Instrument parameter/output determination
  - **Probe Characterization**
- Data acquisition by experiment
  - **Motor-controlled mechanical scans**
    - **“Stop-and-Go” scan preferred**
  - Digital data acquisition
    - **No saturation**
  - **Multiple-pass acquisitions with averaging**

# Focal Points of Validation Protocol (contd.)

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- Data simulation by modeling
  - What output signals to compute
  - How to determine input parameters
    - Probe geometry and parameters
    - Sample geometry and parameters
  - How to use simulation output
- Mapping predictions to experimental data space
  - From impedance plane to horizontal-vertical plane
    - Transfer function = complex number (“gain & phase”)
    - Determined by calibration (e.g. notch, controlled lift off)

# Outline

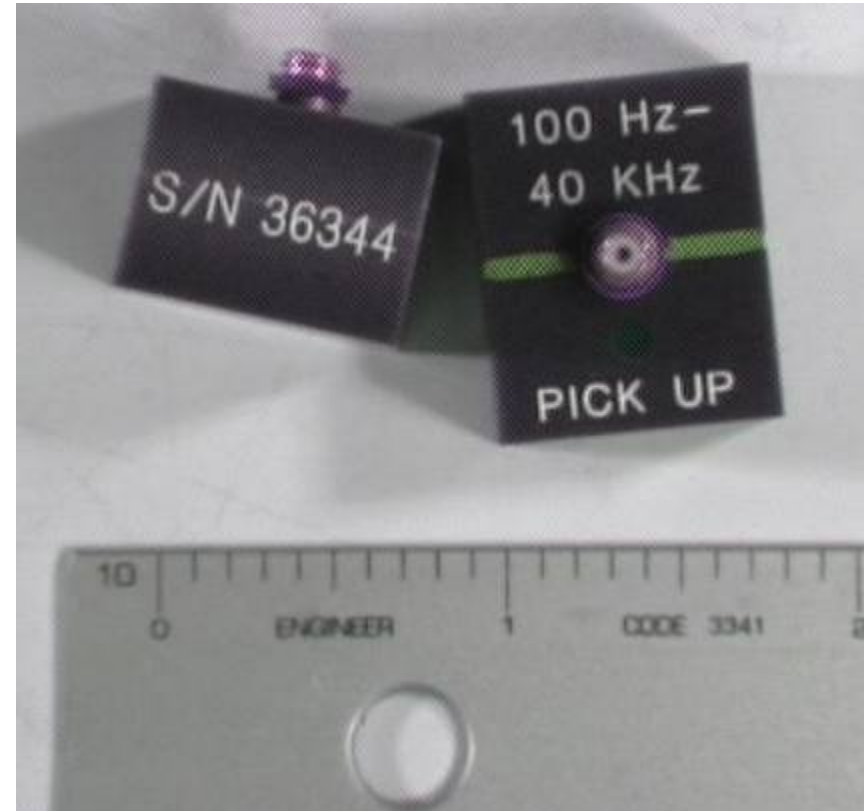
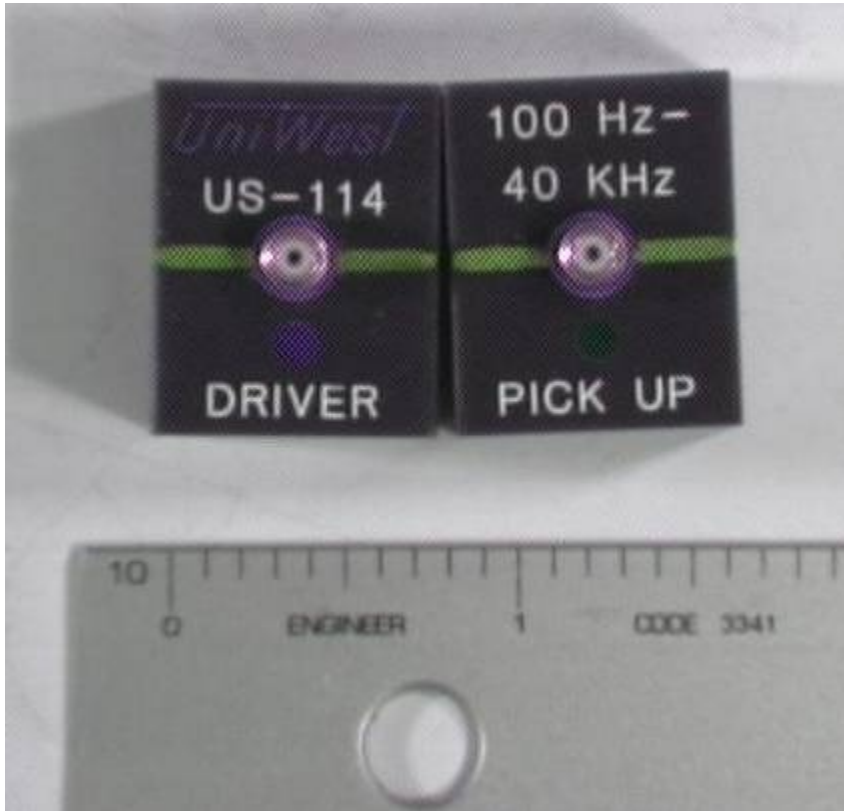
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# Instruments and Specimen

- Instrumentation: A commercial sliding probe (UniWest US-114) attached to EC instrument (US-454)
- Specimen: a custom-made double-layer specimen.
  - The top layer = a 1.016 mm (0.040") thick Al2024-T3 sheet  
The bottom layer = a 6.350 mm (0.250") thick Al 7075-T76 plate
  - The conductivities, 19.31 MS/m (top), 23.77 MS/m (bottom)
  - Two rows of EDM notches in the bottom (Al 7075) plate.
    - 0.127 mm (0.005") opening width, 2-to-1 (L-to-D) aspect ratio
    - Three semi-elliptical notches  
length = 1.524 mm (.060"), 2.540 mm (.100"), 3.810 mm (.150")
    - Four square notches  
length = 1.524 mm (.060"), 2.540 mm (.100"), 3.810 mm (.150"),  
5.080 mm (.200") (through thickness)

# Sliding Probe



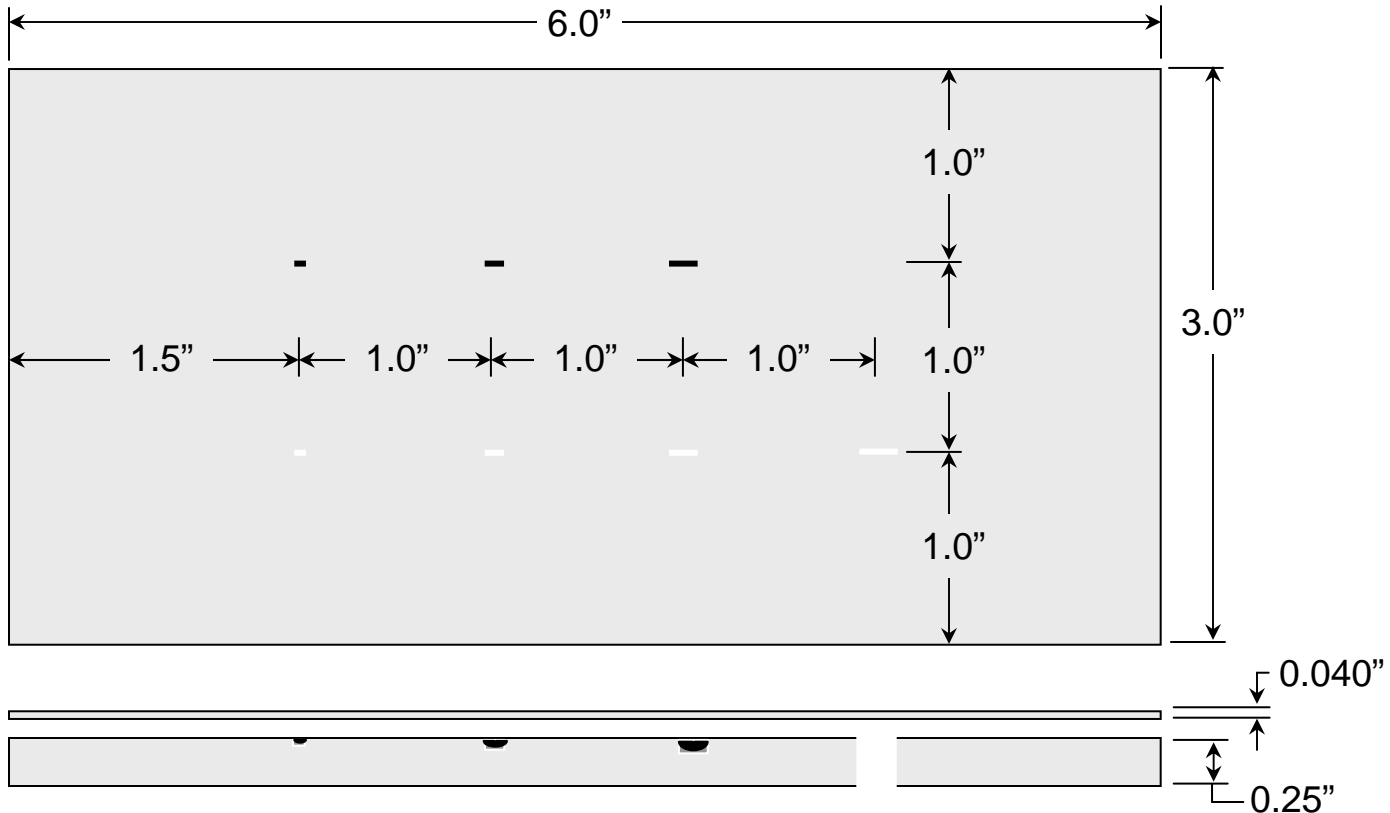
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# Case II Specimen

Material: 2024-T3 Sheet and 7075-T76 Plate



	Notch 1	Notch 2	Notch 3	Notch 4
Row 1 (Semi-elliptical)	0.060" long x 0.030" deep	0.100" long x 0.050" deep	0.150" long x 0.075" deep	
Row 2 (Square)	0.060" long x 0.030" deep	0.100" long x 0.050" deep	0.150" long x 0.075" deep	0.200" long x 0.25"

Make notch width as narrow as possible but 0.007" Max.

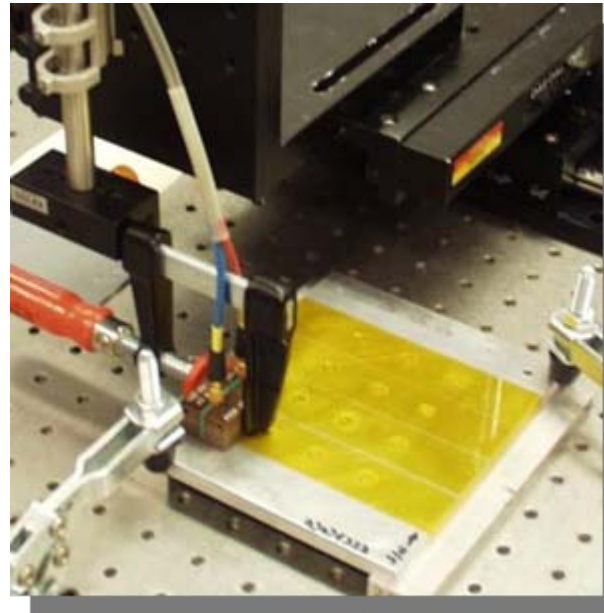
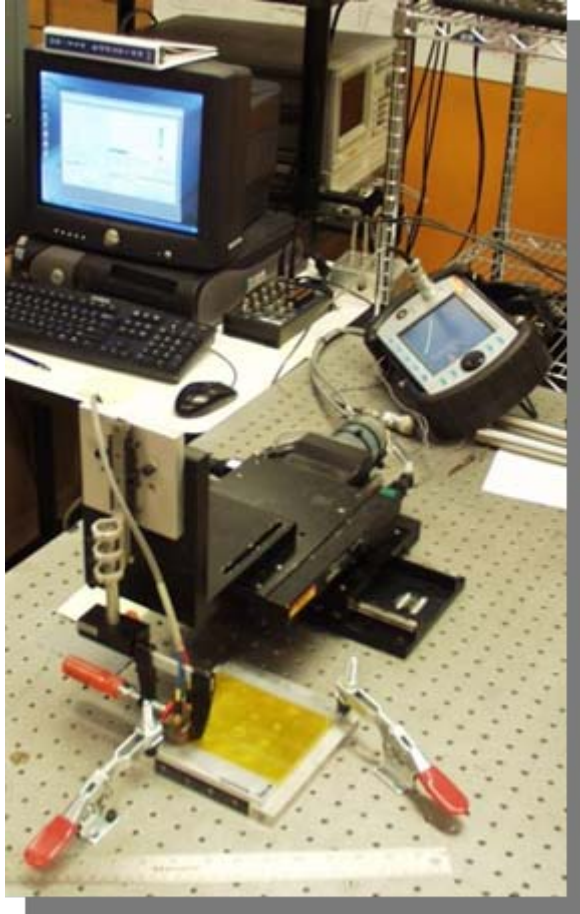
# Case II Specimen Overall Photo



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# Automated Scanner-DAQ Station



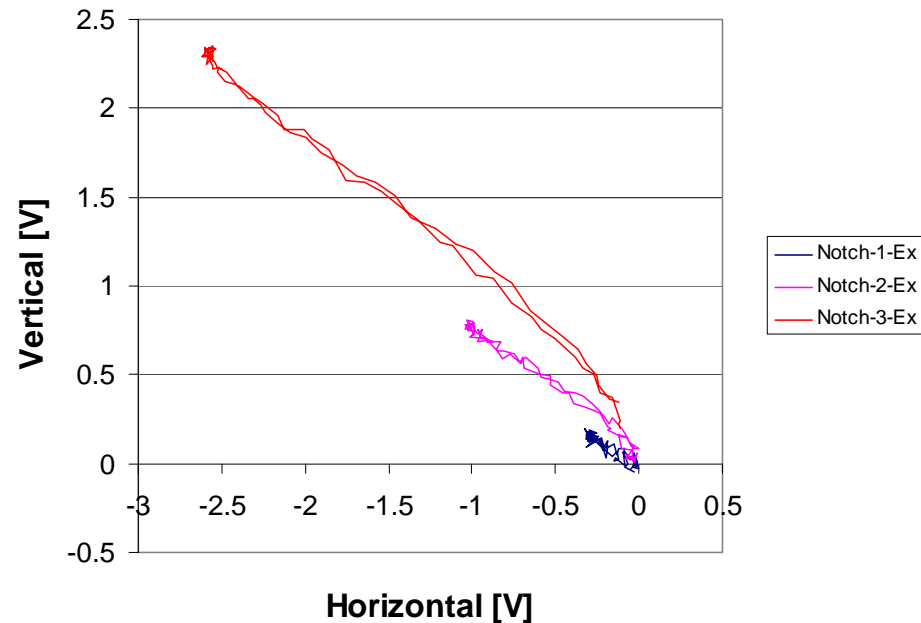
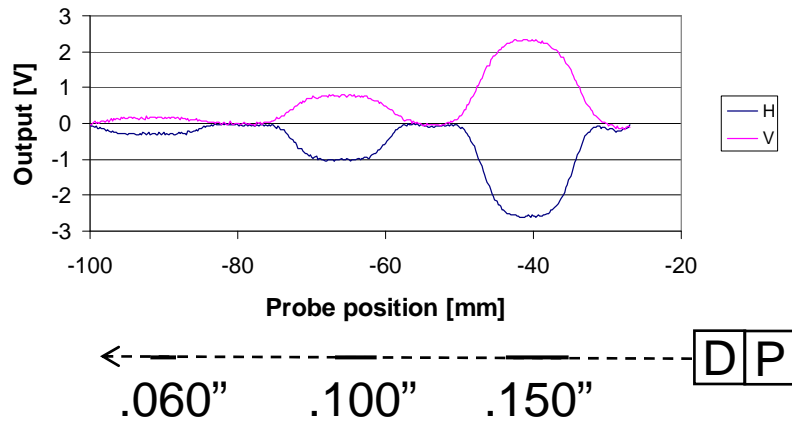
Scan Setup for Validation Specimens

# Experiment

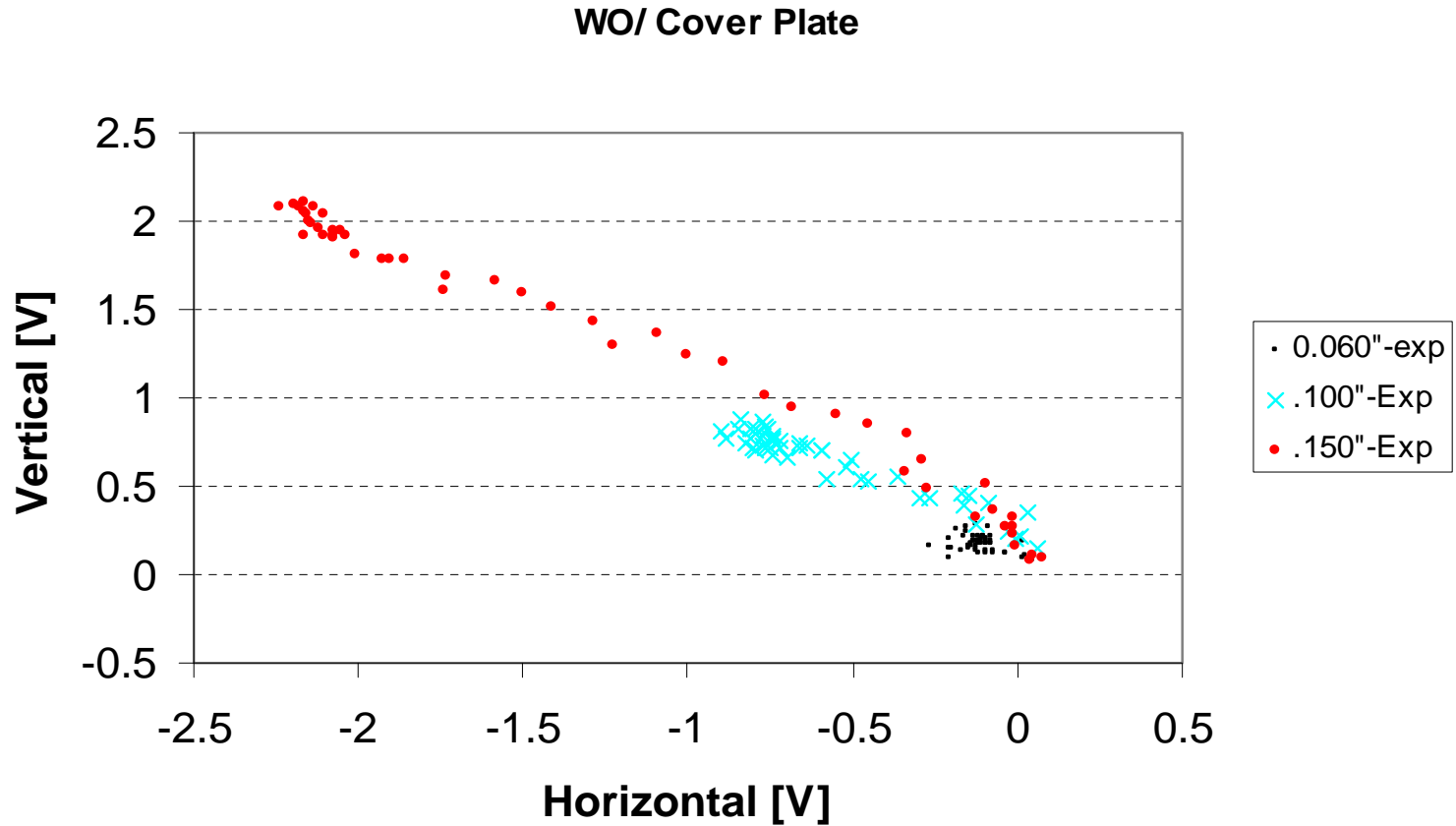
- The physical probe was
  - connected to the eddy current instrument (UniWest US-454)
  - mounted to our computer-controlled scanning system
  - and scanned over the notches, with the output voltages being digitized and acquired.
- The data were acquired for all the four possible plate configurations
  - notches on the probe side or the opposite
  - with or without the top sheet.
- Two data sets used
  - the notches on top, without the top sheet.
    - the instrument settings = 1 kHz, 65.0 dB, and 55°
  - the notches on top, with or without the top sheet.
    - the instrument settings = 1 kHz, 69.0 dB, and 30°

# Typical Experimental Data, Case II Sample

- Without top sheet
- Sliding probe data
- US-454, Gain = 65dB, Phase = 10°

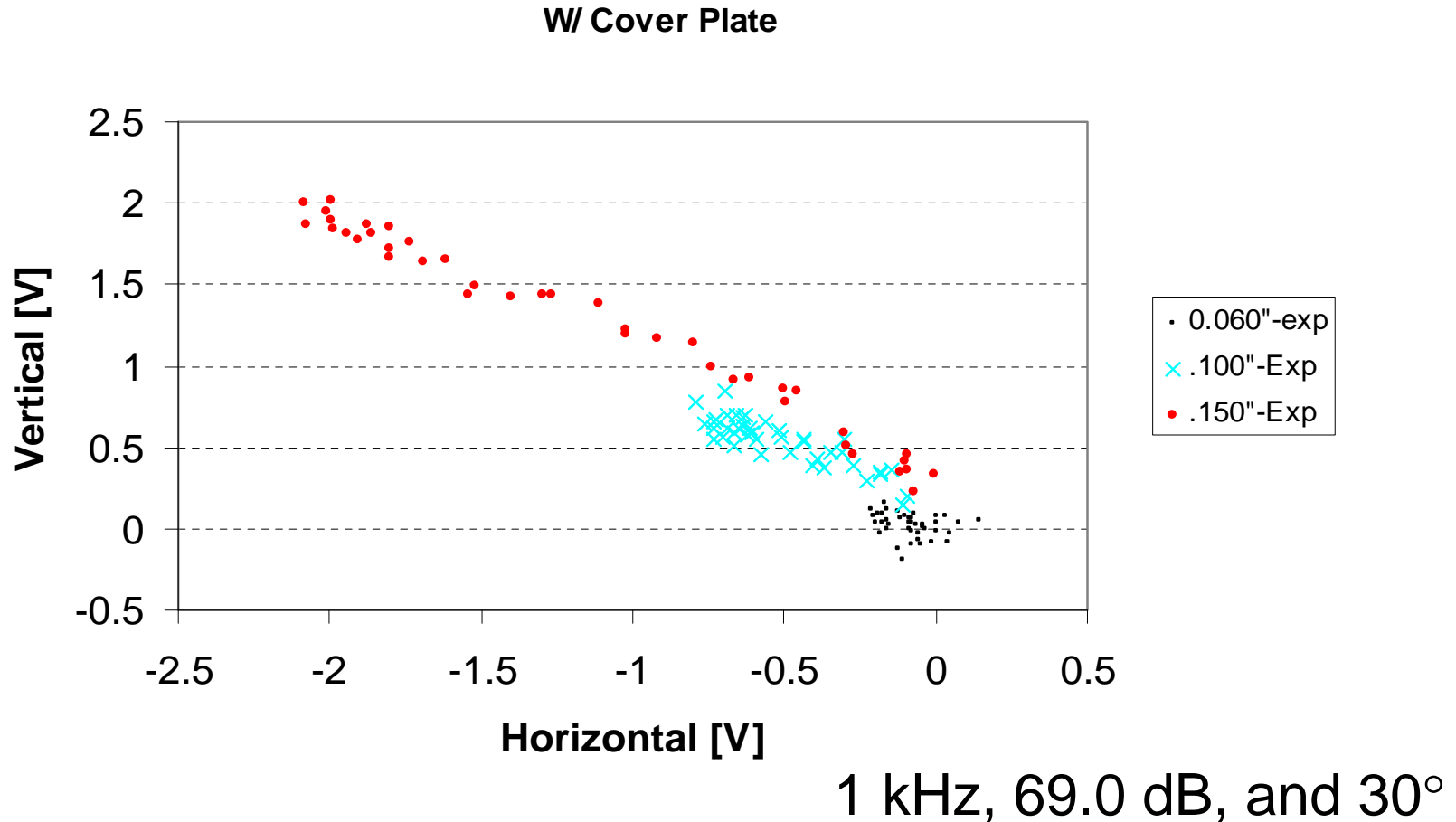


# Data, No Top Sheet



1 kHz, 65.0 dB, and 55°

# Data, with Top Sheet

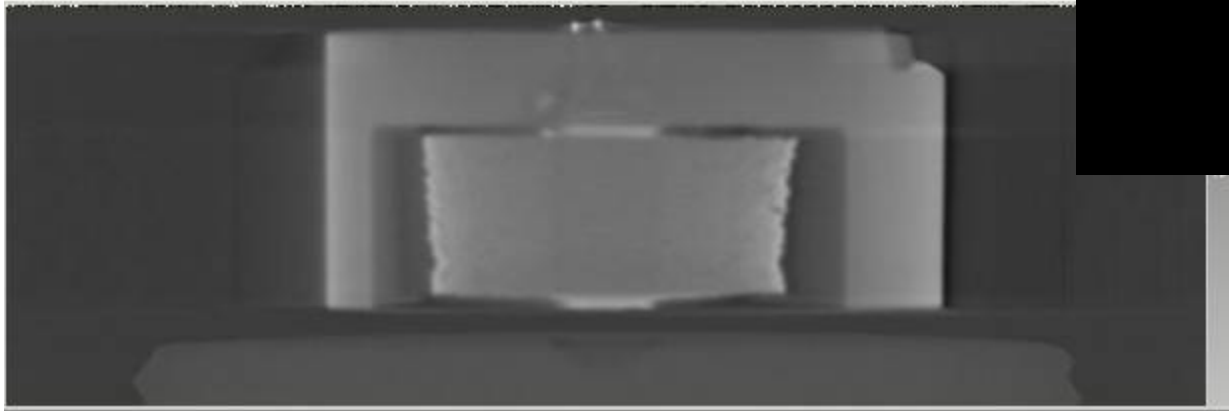
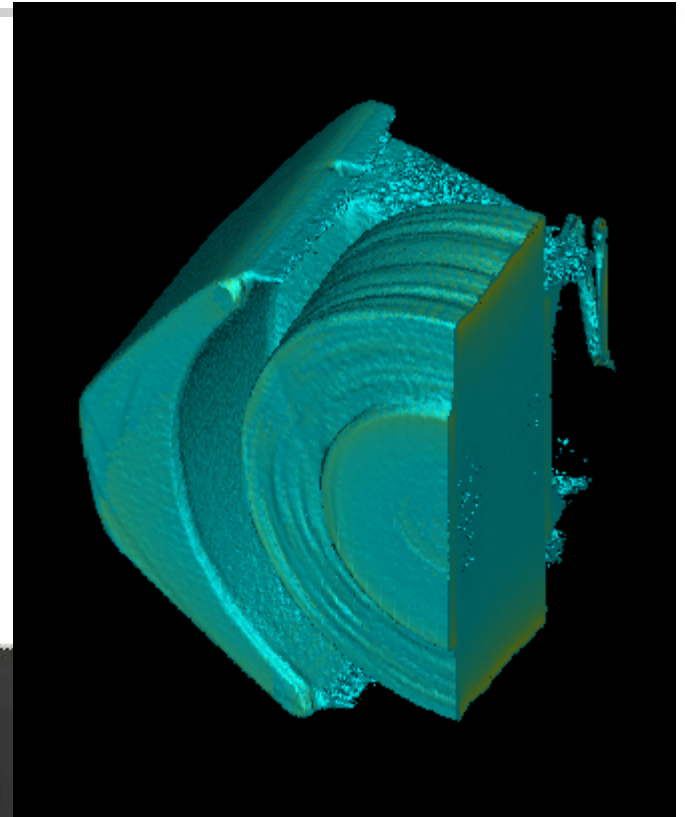
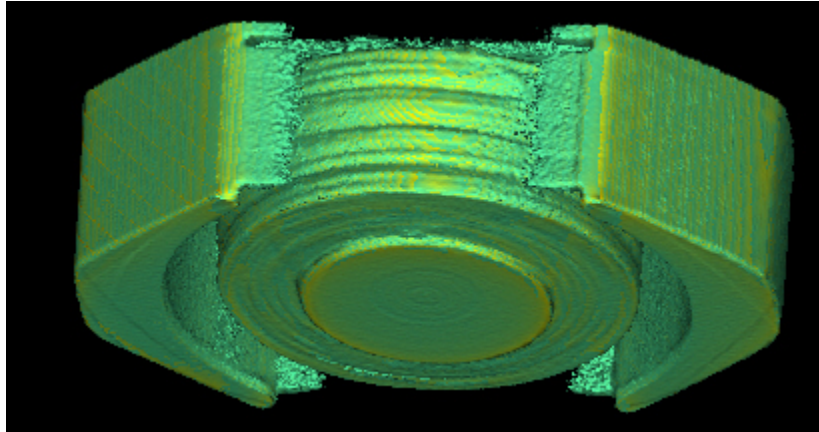


# Computations

- The impedance predictions via PLATE07
  - The two corresponding configurations of the plates and notches
  - A CAD model of the probe obtained from the x-ray images
  - The other specimen parameters as input
    - Ex. the overall lift off = 0.53 mm
- The model output are complex impedance values
  - Need to be mapped to the vector-voltage values to compare the experimental data.
  - A single, multiplicative transfer function
    - for a given frequency (e.g. 1 kHz) and for a given lift-off value (e.g. 0.53 mm).
  - The single multiplicative complex factor can be determined by calibration.
    - In this example; calibration via the maximum of the .150” notch signal
    - The single (complex-valued) scaling factor was used in what follows.



# CT Images of Driver Coil

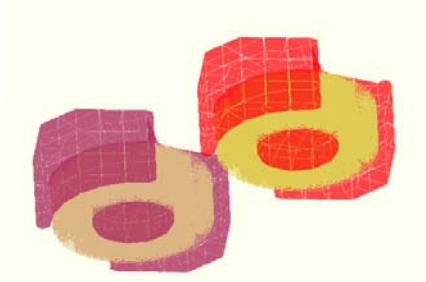
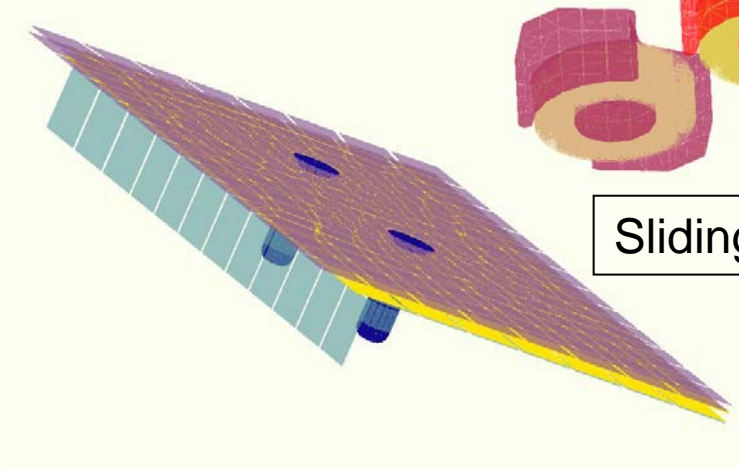


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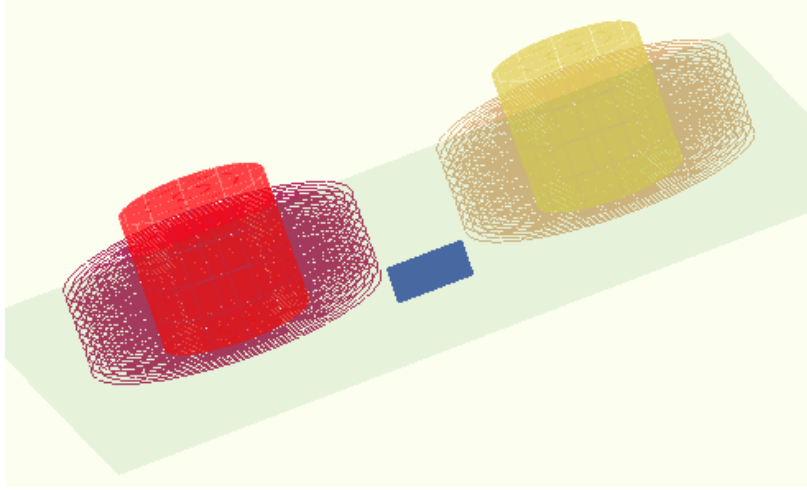
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# CAD Model of the Probe

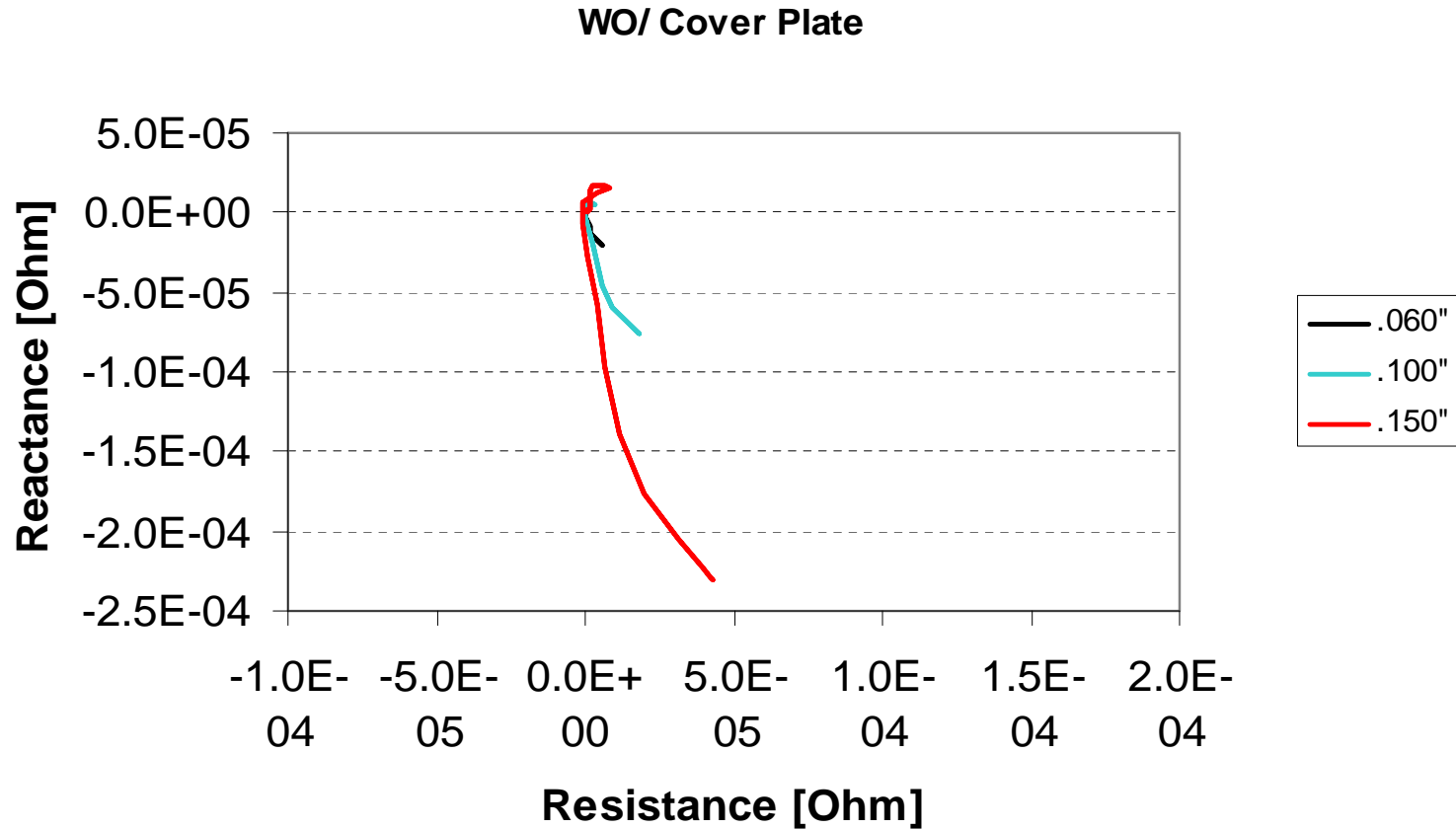
Capture geometry/dimension data



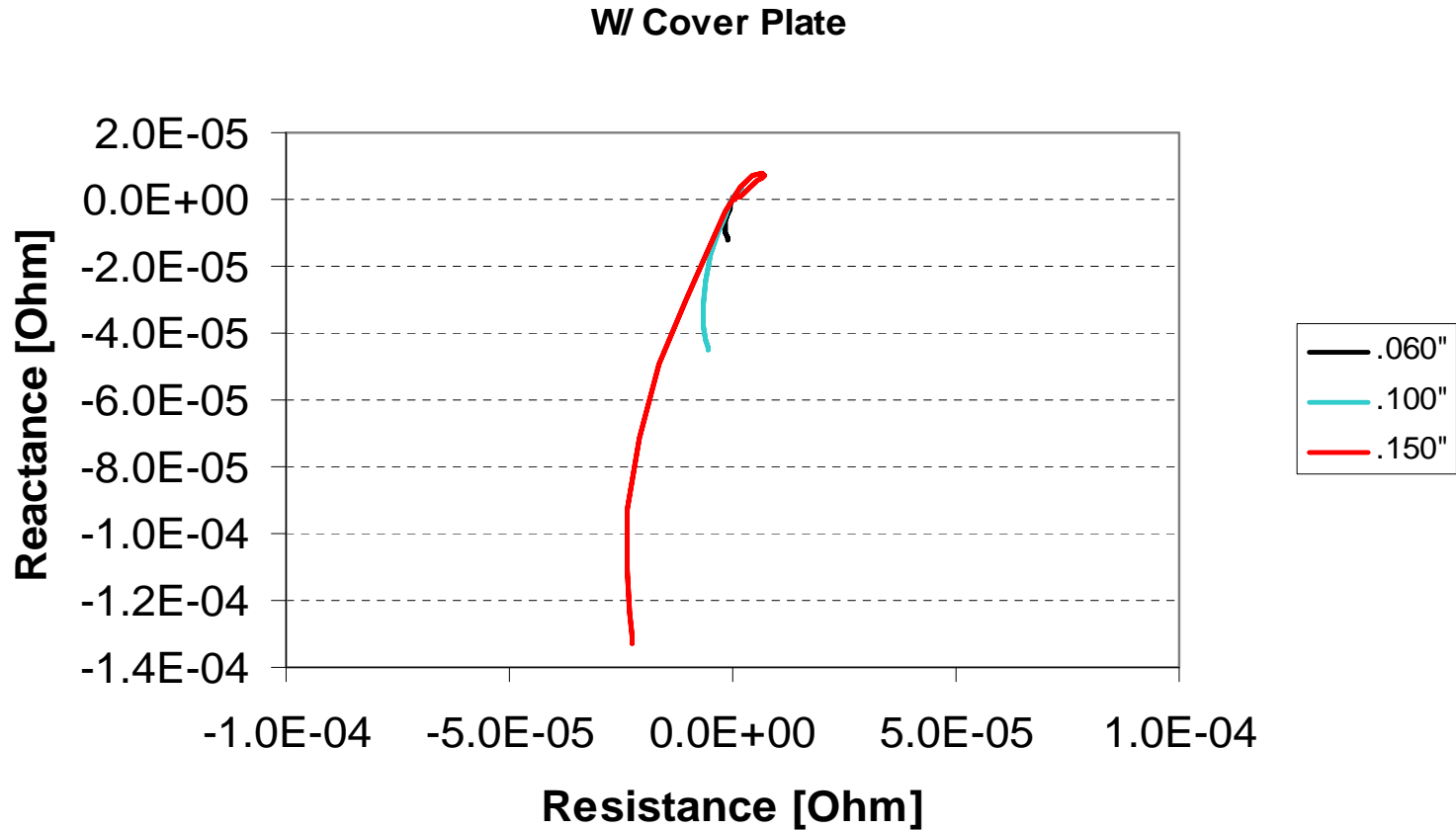
Sliding Probe



# Signal Prediction, no Top Sheet

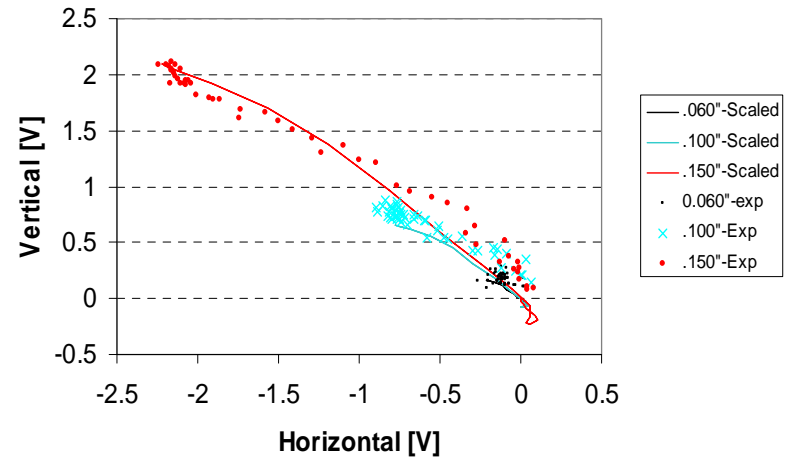
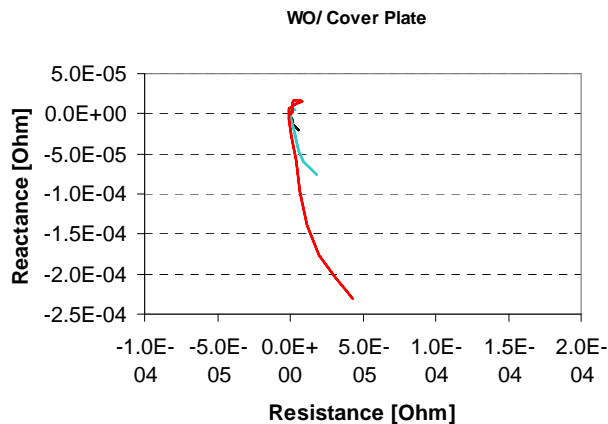
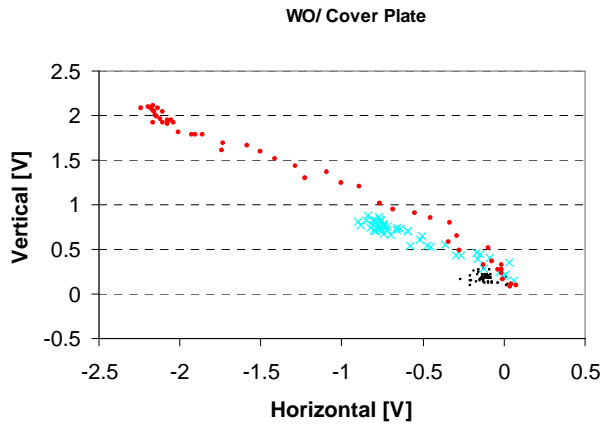


# Signal Prediction, with Top Sheet

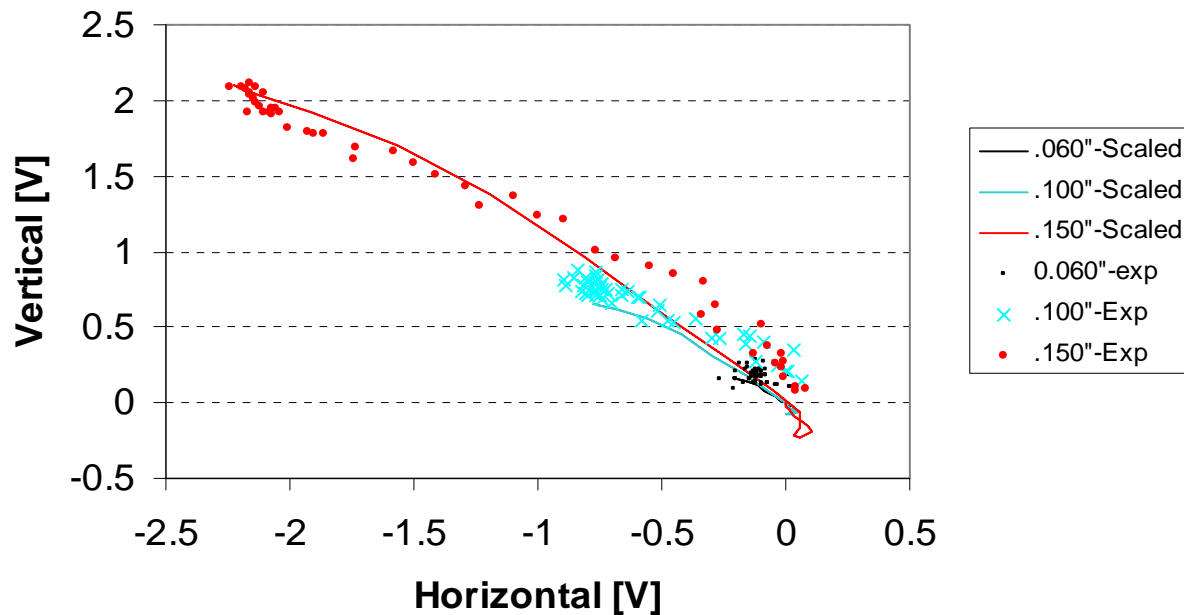


# Mapping Theory to Instrument Output

- Calibration-based approach

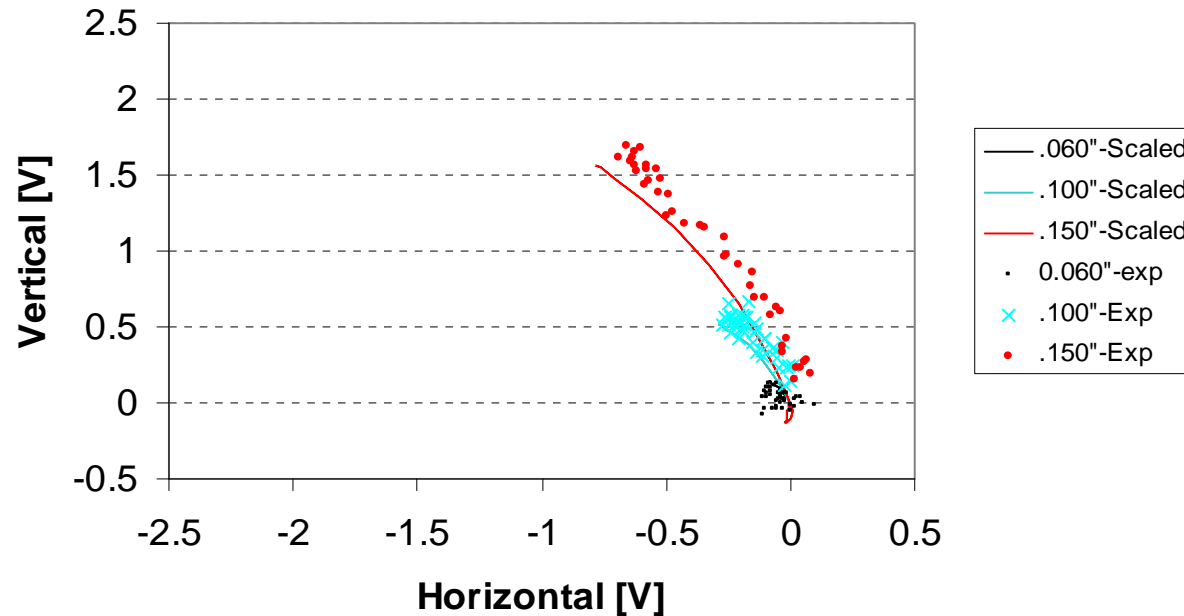


# Model vs Data, No Top Sheet



Vector-voltage plane plots of the three 2-to-1 notch signals without the top sheet. The dots represent measured values (the instrument settings of 1 kHz, 65.0 dB, and 55°). The lines represent scaled model predictions. A single complex number (i.e. magnitude and a phase) was determined so that the maximum .150" signal matches the corresponding experimental maximum, and used to map the predicted impedance to the voltage plane.

# Model vs Data, with Top Sheet



Vector-voltage plane plots of the three 2-to-1 notch signals with the .040" top sheet. In plotting the measurement data (dots), the acquired data at 1 kHz, 69.0 dB, and 30° were scaled/rotated by 4dB and 25° to match the 65.0 dB, and 55° settings. For the theory curves, the same complex scale factor determined previously was used to map the impedance prediction to the plotted voltage curves, as represented by the lines.

# Conclusions

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- A version of model validation protocol document has been developed.
  - Eddy current inspection and modeling
  - Draft
- A case study of exercising the draft validation protocol has been shown.
- Explicit validation results are emerging
  - Ex. Case II sample with sliding probe scans